



### **CFD Team Simulations for CAST**

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46<sup>th</sup> CAST Collaboration Meeting 26-28/09/2011









□ What`s happening inside the magnet?

- A) Updates on thermal boundary conditions
- B) Updates on helium-3 properties
- □ Test cases
- CFD model
- □ Validation
- □ Sample results
- □ Future work





 $\Box$  Because of heat conduction from the outer environment through the solid parts, the temperature of the window wall is higher than the cryostat set point.

□ Natural convection occurs at the window and helium-3 is heated up.

 $\Box$  Hot & light helium enters the cold bore, is cooled down, falls to the bottom of the cold bore and comes back to the window.

□ The heat entering the fluid at the window is given back to the cryostat at the cold bore.

□ The phenomenon is due to the huge dependence of density on temperature.





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#### **Updates on thermal boundary conditions**





#### **Updates on Helium-3 properties**



□ The  $c_p$  vs *T* correlation provided to the CFD Team was wrong (data reduced from Huang Y., Chen G., Arp V., Debye equation of state for fluid helium-3, Journal of Chemical Physics 125, 054505 (2006)).

□ The revised  $c_p$  used in the CFD simulations is computed by means of a preliminary Helmholtz equation of state for Helium-3 of Lemmon E.W. (2002) [REFPROP NIST, Boulder, CO, USA].



CFD team





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□ Steady-state

#### Horizontal position

#### "Cold windows":

Pressure	T_cold bore	T_WF1	T_WF2	T_WR1
[mbar]	[K]	[K]	[K]	[K]
43.65	1.73	20.0	18.3	13.2
67.50	1.73	19.5	17.8	11.5
83.39	1.76	19.0	16.5	11.2
97.60	1.73	18.5	17.3	10.4

#### "Hot windows":

Pressure [mbar]	T_cold bore	Tw_MFB1	Tw_MFB2	Tw_MRB1	Tw_MRB2
	1.00				
14.35	1.80	63.5	/0.0	64.5	66.5
26.40	1.85	68.5	72.5	68.7	72.1
37.10	1.80	61.8	64.3	60.6	64.8







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#### **CFD Model**



- □ Heat conduction occurs in the wall.
- □ Natural convection problem, strong coupling with energy equation.
- Turbulence must be taken into account.
- $\Box$  Strong dependence of density, viscosity,  $c_p$  and conductivity on temperature.
- □ High accuracy is required.



- □ Coupled solver (i.e. energy and Navier Stokes equations are solved together).
- □ Turbulence model: low-Re k- $\omega$  SST without wall function.
- $\Box \text{ Mesh size} \sim 9 \ 10^6 \text{ cells.}$









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#### "Cold windows":

Pressure	Experimental mass	CFD mass	Deviation
[mbar]	[mol]	[mol]	[%]
43.65	9.49	9.54	0.5
67.50	15.18	15.28	0.6
83.39	18.89	18.91	0.1
97.60	23.11	23.19	0.3

#### "Hot windows":

Pressure [mbar]	Experimental mass [mol]	CFD mass [mol]	Deviation [%]
14.35	2.78	2.81	0.9
26.40	4.98	5.04	1.3
37.10	7.37	7.33	-0.6





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#### **Temperature distribution** (p = 43 mbar)





MRB temperature section.

MFB temperature detail.





#### **Influence of pressure**



Natural convection is due to the dependence of density on temperature.
 At higher pressure the density change is larger.



 $\Box$  At higher pressure the natural-convection phenomenon is stronger and the region with non-uniform density is wider.





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#### **Future Work**



□ Transient simulations for the magnet tilting process are needed. The present computational approach is too demanding to perform a transient simulation for the tilting magnet case  $(1 \sim 2 \text{ weeks to get convergence for steady-state simulations}).$ 



• A "lighter" computational approach will be tested for the steady-state horizontal magnet case:

- -) segregated solver instead of coupled solver.
- -) lower number of cells.

□ If possible, the "light model" will be used to solve the unsteady tilting case.







# Thank you

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46th CAST Collaboration Meeting, 26-28/09/2011

